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吊耳焊缝应力分析及其结构设计

吴和保¹,龙玉阳¹,胡汉华²,余经炭²

(1. 武汉工程大学机电工程学院,湖北 武汉 430074;2. 武汉纽威制药机械有限公司,湖北 武汉 430065)

摘 要:为探究吊耳根部焊缝开裂现象,采用有限元分析软件对吊耳焊缝的应力应变过程进行分析,得到焊缝截面上的应力分布规律,罐身直径1 400 mm的中药提取罐吊耳根部焊缝承受最大拉应力为148.98 MPa,其大于焊缝许用应力,焊缝易产生裂痕.通过加入补强筋板的方式,使其危险截面最大应力值降至77.08 MPa,有效地预防了焊缝开裂.

关键词:焊缝;应力;有限元分析

中图分类号: TB115

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0 引言

提取罐吊耳是开门机构驱动的支撑部件,它通过自动控制的气缸实现罐体卸料门的开启和关闭.卸料门的开关过程中,吊耳承受着较大的交变应力作用,工程实践中,常常容易出现吊耳底部与筒壁焊接处焊缝开裂现象,严重影响提取罐的正常运行和操作安全.提取罐属于压力容器,设备运行安全系数要求较高,焊缝开裂的预防就显得尤为重要,为了准确预测开裂源的位置,本文通过力学计算和有限元软件全面分析研究了吊耳根部焊缝的应力分布特征和裂纹形成机理,确立了应力大小与焊缝尺寸的关系,并提出了防止焊缝开裂的优化设计方案.

1 吊耳根部焊缝强度分析

卸料门的开关过程是一个匀速运动,中药提取完成后,容器内部压力卸除,锁紧缸快开开关打开瞬间,吊耳根部所受拉应力最大.如图1所示.

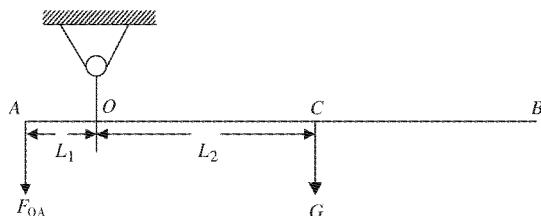


图1 排渣门受力简图

Fig.1 Free-body diagram of slagging door

由杠杆平衡条件得:

$$F_{QA} \cdot l_1 = G \cdot l_2$$

$$F_{QA} = \frac{l_2}{l_1} G = \frac{830 \times 10^{-3} \times 2 \times 453.8}{95 \times 10^{-3}} = 31\,439 \text{ N}$$

以启闭缸吊耳为研究对象,现对其进行受力分析,作用在吊耳上的力 F_{QA} ,表现形式为对吊耳的弯矩,吊耳与补强板的焊接方式为连续角焊,焊缝宽度为6 mm,焊缝截面为矩形框,如图2所示.

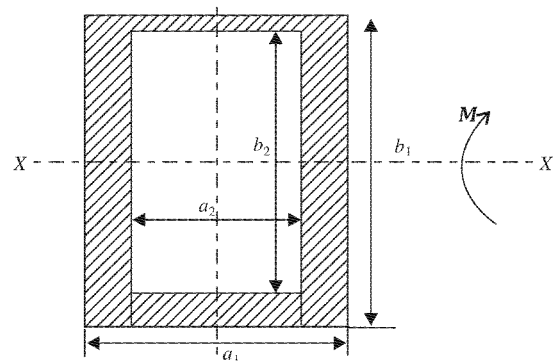


图2 焊缝截面图

Fig.2 Diagram of weld section

矩形框惯性矩为

$$I_x = \frac{a_1 b_1^3}{12} - \frac{a_2 b_2^3}{12} = \frac{0.066 \times 0.196^3 - 0.054 \times 0.184^3}{12} \text{ m}^4 =$$

$$1.34 \times 10^{-5} \text{ m}^4$$

抗弯截面系数^[1]:

$$w_x = \frac{I_x}{y_{\max}} = \frac{1.34 \times 10^{-5}}{0.098} \text{ m}^3 = 1.37 \times 10^{-4} \text{ m}^3$$

最大拉、压应力:

$$\sigma = \frac{M_{\max}}{w_x} = \frac{21\,439 \text{ N} \times 0.238 \text{ m}}{1.37 \times 10^{-4} \text{ m}^3} = 37.24 \text{ MPa}$$

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作者简介:吴和保(1963-),男,湖北麻城人,教授,博士.研究方向:铸造合金材料及成形工艺.

根据强度设计准则: $\sigma \leq \frac{[\sigma]}{n}$

其中: σ 为角焊缝许用应力, n 为安全系数. 查表^[1]得: 角焊缝拉伸、压缩、弯曲许用应力 $[\sigma] = 118 \text{ MPa}$, 安全系数按抗断裂计算取 $n = 4$.

那么 $\sigma \cdot n = 148.98 \text{ MPa} > [\sigma]$

该截面处的理论拉应力大于许用应力, 该截面是危险截面, 且根据焊缝断裂原因以及弯矩的作用形式, 分析知最大拉应力位于矩形框下截面.

2 基于有限元软件的吊耳根部焊缝模拟

为了深入分析焊缝产生裂痕原因, 采用有限元软件建模^[2-4], 进行网格划分和有限元的计算, 得出吊耳根部应力分布图, 如图 3 所示. 其中, 吊耳尺寸为 $238 \times 180 \times 50$, 底板尺寸为 $320 \times 180 \times 8$, 材料均为 Q235, 吊耳与底板采用角焊形式, 焊条牌号 J427, 焊缝高度为 8 mm.

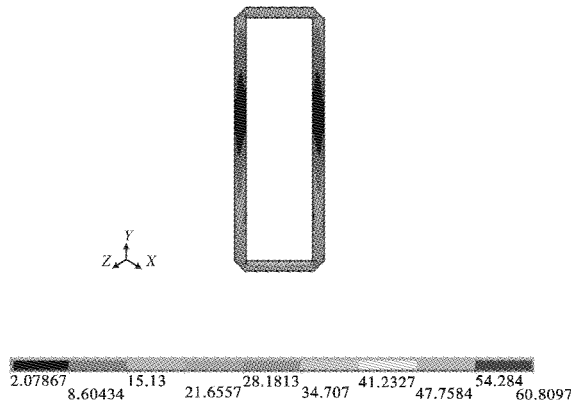


图 3 焊缝截面应力分布图

Fig. 3 Diagram of stress distribution on weld section

由上图分析可知, 由于受转矩作用, 矩形焊缝框一端受拉应力作用, 一端受压应力作用, 且最大应力位于矩形框下端, $\sigma_{\max} = 60.8097 \text{ MPa}$, 与理论分析相符.

3 防止焊缝开裂的措施

在最危险截面处, 增加一块补强筋板. 如图 4 所示.

加上补强板后, 整个焊接截面如图 5 所示.

该截面的惯性矩 I_x 由下面公式算得:

$$I'_x = \frac{1}{3}(Be_1^3 - bh^3 + ae_2^3) =$$

$$\frac{1}{3}(0.1 \times 0.09^3 - 0.05 \times 0.082^3 + 0.05 \times$$

$$0.098^3) \text{ m}^4 = 0.000030797 \text{ m}^4$$

$$I''_x = \frac{1}{3}(Be_1^3 - bh^3 + ae_2^3) =$$

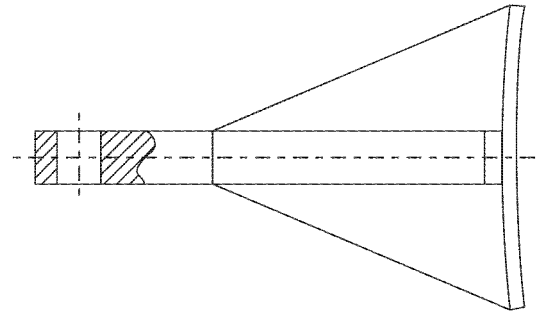


图 4 吊耳俯视图

Fig. 4 Vertical view of lifting lug

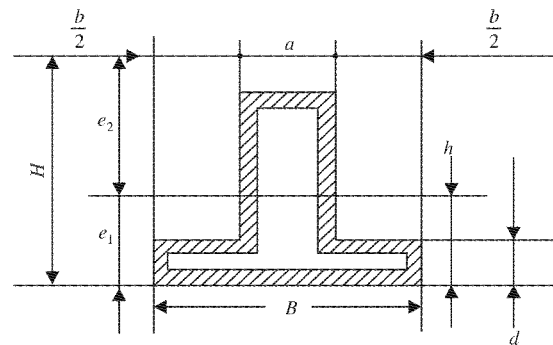


图 5 焊缝截面图

Fig. 5 Diagram of weld section

$$\frac{1}{3}(0.116 \times 0.094^3 - 0.05 \times 0.07^3 +$$

$$0.066 \times 0.11^3) \text{ m}^4 = 0.000055681 \text{ m}^4$$

$$I_x = I''_x - I'_x =$$

$$0.000055681 \text{ m}^4 - 0.000030797 \text{ m}^4 =$$

$$0.000024884 \text{ m}^4$$

该截面的抗弯截面系数:

$$W_x = \frac{I_x}{e_1} = \frac{0.000024884 \text{ m}^4}{0.094 \text{ m}} =$$

$$0.000264723 \text{ m}^3$$

最大拉应力:

$$\sigma_{\max} = \frac{M_{\max}}{W_x} = \frac{21439 \text{ N} \times 0.238 \text{ m}}{0.000264723 \text{ m}^3} =$$

$$19.27 \text{ MPa}$$

根据强度设计准则 $\sigma \leq \frac{[\sigma]}{n}$ 计算:

$$\sigma \cdot n = 77.08 \text{ MPa} < [\sigma]$$

加了补强板之后, 适当的增加了焊缝的面积, 增大了抗弯截面系数, 危险截面的最大拉应力由 148.98 MPa 降至 77.08 MPa, 对吊耳与补强板焊缝的抗裂起到很大程度上的帮助.

4 结 语

通过理论计算和有限元软件建模两种途径分析了中药提取罐启闭缸吊耳的焊缝强度问题, 得到以下结论:

(1) 经计算, 吊耳根部矩形焊缝截面的截面系

数为 $1.37 \times 10^{-4} \text{ m}^3$, 最大拉应力为 148.98 MPa, 大于许用应力值, 该截面为危险截面, 容易开裂。

(2) 运用有限元软件对矩形焊缝截面进行了数值模拟, 其上应力分布为: 从矩形框中部向两端, 应力值逐渐增大, 最大应力集中于矩形框最底部。

(3) 通过在吊耳底部增设一个补强筋板, 使其危险截面最大应力值降至 77.08 MPa, 有效地预防了焊缝开裂。

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Analysis of stress and structure design in lifting lug welding

WU He-bao¹, LONG YU-yang¹, HU Han-hua², YU Jing-tan²

(1. School of Techtronic Engineering, Wuhan Institute of Technology College Wuhan 430074, China;

2. Wuhan Newway Pharmaceutical Machine Limited Company, Wuhan 430065, China)

Abstract: In order to explore the crack at the end of lifting lug, the finite element analysis software was used to analyze stress-strain process of lifting lug welding and stress distribution on weld section was displayed. When diameter of can-body is 1400 millimeter and maxximum tensile stress of weld at the end of lifting lug is 148.98 MPa, which is greater than the allowable tensile stress, the crack at the weld seam is formed easily. By using reinforcement plate, the maximum tensile stress on weld dangerous section decreased to 77.08 MPa to prevent weld cracking effectively.

Key words: weld; stress; finite element analysis

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Prediction analysis of upstream gasification via technique of intermittent gasification and oxygen enrichment

ZHANG Li¹, LIU Sheng-li¹, DING Yao², ZHANG Feng-kui³, HUANG Pu¹

(1. School of Environment and Civil Engineering, Wuhan Institute of Technology, Wuhan 430074, China;

2. School of Chemical Engineering and Pharmacy, Wuhan Institute of Technology, Wuhan 430074, China;

3. Wuhan Engineering Co., Ltd, Wuhan 430073, China)

Abstract: To solve the current problem of high energy consumption in the upstream gasification, we developed a technique of generating ammonia synthesis feed gas using intermittent gasification and oxygen enrichment during the process of upstream gas production. In order to predict the effects of oxygen gas on the upstream gasification via oxygen enrichment and gasification, a company in Sandong was taken as an example. Before technical transformation, natural gas air (79% nitrogen and 21% oxygen) was added in the gas making process. After the technical transformation, steam entering the gasifier including 90% oxygen and 10% nitrogen was used to meet the requirement of $(\text{CO} + \text{H}_2)/\text{N}_2$. Because the heat of steam decomposition in the endothermic reaction was made up, steam was decomposed in high temperature conditions for a long time. The results show that the rate of steam decomposition and the efficiency of coal utilization are improved, the emission of carbondioxide and sulfur dioxide is reduced.

Key words: upstream gasification; oxygen enrichment and gasification; consumption reduction; forecast

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